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## PROCESSES AND APPARATUSES FOR TREATING HALOGEN-CONTAINING GASES

### Field of the Disclosure

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The present disclosure relates to processes and apparatuses for treating halogen-containing gas, particularly fluorine gas.

### Background

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Halogen-containing gases are environmental hazards and must be removed or reduced from emission sources. Treatment of fluorine gas ( $F_2$ ) is especially problematic since it is only marginally soluble in water and, thus, cannot be efficiently removed from an effluent stream via water scrubbing. The solubility in water is also poor for other halogen-containing gases such as trichloroethylene, chloroform, perchloroethylene, various chlorofluorocarbons ("CFCs"), and various perfluorinated carbons ("PFCs"). Effluent streams from semiconductor manufacturing often contain such halogen-containing gases.  $F_2$  is of particular interest since it is becoming more common as an emission product from  $NF_3$  - based dielectric chamber cleaning processes.

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Conventional treatment of  $F_2$  gas involves combustion with a fuel gas (e.g., natural gas or butane) at 700-800°C in a burn box resulting in the formation primarily of hydrogen fluoride (HF), carbon dioxide ( $CO_2$ ) and water. In addition to the high heat requirements and the need for a fuel gas, the conventional treatment method suffers from corrosion problems since the formed HF is highly corrosive at such high temperatures.

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An alternative thermal process for destroying  $F_2$  involves reacting the  $F_2$  gas with steam in the presence of an oxidation source (e.g., air) (see Flippo et al., "Abatement of Fluorine Emissions Utilizing an ATMI CDO™ Model 863 with Steam

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Injection" (<http://www.semiconductorsafety.org/meetings/proc2001/20.pdf>)).

According to this article, the steam acts as a reducing agent for reducing the F<sub>2</sub> gas into HF.

Treatment of various halogen-containing gases other than F<sub>2</sub> via plasma reactions have also been disclosed. For example, U.S. Patent No. 5,187,344 describes decomposing CFCs or trichloroethylene by reacting the CFC or trichloroethylene with water in the presence of a thermal plasma. U.S. Patent No. 6,187,072 B1 describes oxidizing PFCs under plasma conditions to produce F<sub>2</sub>. Grothaus et al., "Harmful Compounds Yield to Nonthermal Plasma Reactor", Technology Today, (pub. Southwest Research Institute Spring 1996) describes treating NF<sub>3</sub> by adding H<sub>2</sub> gas and passing the resulting mixture through a pulsed corona non-thermal plasma reactor. The products were said to be F<sub>2</sub> and HF.

So-called "point-of-use" plasma abatement of PFCs in semiconductor processing effluent streams has also been described (see, e.g., Vartanian et al., "Plasma Abatement Reduces PFC Emission", Semiconductor International, June 2000, (hereinafter "Vartanian") and "Evaluation of a Litmas "Blue" Point-of-use (POU) Plasma Abatement Device for Perfluorocompound (PFC) Destruction", International SEMATECH, Technology Transfer #98123605A-ENG (1998) (hereinafter "SEMATECH disclosure"). Point-of-use abatement involves placing a high-density plasma source ( $n_e > 10^{12}/\text{cm}^3$ ) in the foreline of a process tool between the turbomolecular and dry pumps. Both Vartanian and the SEMATECH disclosure mention that H<sub>2</sub> could be an additive gas in the plasma.

Despite these efforts, a need continues to exist for efficient methods and apparatuses for treating halogen-containing effluent gases that operate at low temperature and atmospheric pressure. Such a need particularly exists for halogen-containing gases that are only marginally soluble in water such as F<sub>2</sub>.

### Summary of the Disclosure

Halogen-containing gases are commonly-occurring emissions from manufacturing or cleaning processes such as etching in semiconductor manufacturing or metal cleaning in automobile manufacturing. Fluorine-laden gases are also a major byproduct from aluminum smelting. The disclosed processes and apparatuses offer an efficient abatement option for substantially decreasing or eliminating the amount of halogen-containing gas released into the atmosphere by industry.

In particular, there are disclosed various processes for treating a halogen-containing gas such as  $F_2$  that involve generating a plasma in order to chemically reduce the halogen-containing gas into products that are more environmentally manageable.

A first embodiment involves providing a treatment gas that includes at least one halogen-containing gas, mixing at least one gaseous reducing agent with the treatment gas resulting in a feed gas mixture, and generating a non-thermal plasma in the feed gas mixture in the presence of a liquid to reduce the halogen-containing gas. The non-thermal plasma may be a silent discharge plasma according to one variant of the first embodiment.

A second embodiment involves providing a treatment gas that includes at least one halogen-containing gas, mixing at least one gaseous reducing agent with the treatment gas resulting in a feed gas mixture, and generating a plasma in the feed gas mixture in the presence of liquid water to reduce the halogen-containing gas.

A third embodiment involves introducing a halogen-containing gas and a gaseous reducing agent into a chamber, introducing a liquid into the chamber, generating a non-thermal plasma in the chamber to reduce the halogen-containing gas, and exhausting the resulting reduction product from the chamber. According to one variant of the third embodiment, the chamber contains at least one electrode and the liquid flows as a film over at least a portion of the electrode.

A fourth embodiment involves providing a chamber defining at least one gas inlet for receiving a feed gas mixture that includes a halogen-containing gas and a

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gaseous reducing agent, and at least one water inlet for receiving liquid water; providing at least one first electrode disposed within the chamber; providing at least one second electrode disposed within the chamber; flowing the liquid water over at least a portion of the first electrode; and applying electric potential to the first and second electrodes so as to generate a plasma in the feed gas mixture and reduce the halogen-containing gas. According to one variant of the fourth embodiment, the first electrode defines at least one second gas inlet for introducing the gaseous reducing agent through the liquid water and into the chamber so as to mix with the halogen-containing gas and form a feed gas mixture.

There is also disclosed a further embodiment for treating fluorine gas that contemplates providing a treatment gas that includes fluorine gas, mixing at least one reducing agent with the treatment gas resulting in a feed gas mixture, and generating a non-thermal plasma in the feed gas mixture to convert the fluorine gas to hydrogen fluoride gas.

Water-soluble gaseous reduction products resulting from these disclosed processes can be dissolved in water for further treatment or recycling rather than discharged into the atmosphere. For example,  $F_2$  gas is only marginally soluble in water. In contrast, the HF gas produced by reduction of  $F_2$  gas is water-soluble and is easily removable from a gas stream via scrubbing.

The liquid present during generation of the plasma can serve a number of purposes. First, it absorbs a significant amount of the heat generated by the exothermic reduction reaction. Accordingly, the operating bulk gas temperatures during the plasma generation do not exceed about  $100^\circ\text{C}$  in many variants of the disclosed processes. Thus, the corrosive effect of the gas phase reduction products is substantially diminished compared to the corrosive effect at the  $700$  to  $800^\circ\text{C}$  operating temperatures of the conventional combustion process. Second, if the liquid is water, the water-soluble gaseous reduction products can dissolve in the water that is present in the plasma reactor. Thus, scrubbing of the reduction product stream can be substantially completed, or at least initiated, in the plasma reactor.

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Also disclosed is a novel plasma reactor apparatus that includes a chamber defining at least one first gas inlet for receiving a first gas, and at least one water inlet for receiving liquid water; at least one first electrode disposed within the chamber and defining a first surface that is in fluid communication with the water inlet for receiving  
5 liquid water, and at least one second gas inlet for receiving a second gas; and at least one second electrode disposed within the chamber and opposing the first surface of the first electrode; wherein a dielectric barrier is disposed on the first surface of the first electrode and/or a surface of the second electrode. Another embodiment of a novel plasma reactor apparatus includes a chamber; means for generating a non-thermal  
10 plasma in the chamber that includes at least one electrode; means for introducing a liquid over at least a portion of the electrode; and means for bubbling or introducing a first gas through the liquid and into the chamber for reaction in the non-thermal plasma.

A further disclosure concerns a system for treating a halogen-containing gas that includes a plasma reactor for reducing halogen-containing gas, a halogen-containing gas  
15 source in fluid communication with the plasma reactor, a reducing agent source in fluid communication with the plasma reactor, and a liquid source in fluid communication with the plasma reactor.

The foregoing features and advantages will become more apparent from the following detailed description of several embodiments that proceeds with reference to  
20 the accompanying figures.

### **Brief Description of the Drawings**

Certain embodiments are described below with reference to the following  
25 figures:

FIG. 1 is a sectional view of one embodiment of a novel non-thermal, film discharge plasma reactor for use in the disclosed processes;

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FIG. 2 is a sectional view of a first embodiment of a novel electrode arrangement in a non-thermal, film discharge plasma reactor for use in the disclosed processes;

FIG. 3 is a sectional view of a second embodiment of a novel electrode arrangement in a non-thermal, film discharge plasma reactor for use in the disclosed processes;

FIG. 4 is a sectional view of one embodiment of a non-thermal plasma reactor for use in the disclosed processes;

FIG. 5 is a schematic of one embodiment of a system that includes the disclosed process;

FIG. 6 is a graph depicting the amount of remaining  $F_2$  vs. applied plasma energy according to examples of one embodiment of the disclosed process; and

FIG. 7 is a graph depicting the amount of remaining  $F_2$  vs. applied plasma energy according to additional examples of one embodiment of the disclosed process.

### Detailed Description of Several Embodiments

The following definitions are provided for ease of understanding and to guide those of ordinary skill in the art in the practice of the embodiments.

“Ambient pressure and temperature” mean pressures and temperatures that typically exist in an environment without any external controls or energy such as a vacuum or heating. Typically, ambient pressure is approximately atmospheric pressure and ambient temperature is approximately room temperature (i.e., about 20 to about 30°C).

“Non-thermal plasma” denotes a plasma having species and particles at very different temperatures. In contrast, a “thermal plasma” denotes a plasma whose species and particles are all at the same temperature.

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"Treatment gas" encompasses any gas or gas mixture that includes at least one constituent that can be destroyed or converted to a more environmentally manageable species via the disclosed processes or apparatuses.

5 Halogen-containing gases that may be treated with the disclosed processes and apparatuses include fluorine gas ( $F_2$ ) and fluorine-containing gases (e.g., PFC, and fluorides such as  $NF_3$ ,  $C_2F_6$ ,  $CF_4$ ,  $SiF_4$  and  $SF_6$ ), chlorine-containing gases (e.g.,  $Cl_2$ , trichloroethylene, chloroform,  $SiCl_4$ ,  $SiCl_2H_2$ , and perchloroethylene), fluorochloro-containing gases (e.g., CFCs), bromine-containing gases (e.g.,  $Br_2$  and brominated hydrocarbons), and iodine-containing gases (e.g., iodated hydrocarbons). The disclosed  
10 processes and apparatuses are particularly suitable as a viable alternative to water scrubbing for gases that are only marginally soluble in water such as  $F_2$ , trichloroethylene, chloroform, perchloroethylene, various CFCs and various PFCs.

The treatment gas may include a mixture of different halogen-containing gases and, optionally, non-halogenated gases such as nitrogen ( $N_2$ ) and inert gases that do not  
15 act as significant reducing or oxidizing agents (e.g., Ar). Oxygen may also be another optional component of the treatment gas. The amount of halogen-containing gas in the treatment gas mixture may vary, for example, from about 0.000001 volume % to about 25 volume %.

The reducing agent may be any material capable of donating hydrogen or an  
20 electron to the halogen-containing gas to effectuate reduction of the halogen-containing gas. Illustrative reducing agents include  $H_2$ , hydrocarbons, ammonia, hydrazines, hydrides (e.g.,  $B_2H_6$  and  $LiAlH_4$ ), amines (e.g., ethylamine and butylamine), amides (e.g., urea and acetamide), water and similar hydrogen-rich materials. Mixtures of such reducing agents could also be employed. An inert gas may also be mixed with the  
25 reducing agent gas. The reducing agent should be in the form of a gas when it is mixed with the treatment gas. However, a liquid reducing agent could be initially provided and then subsequently vaporized for mixing with the treatment gas. According to certain embodiments, a non-aqueous, gaseous reducing agent is mixed with the treatment gas. A non-aqueous, gaseous reducing agent may substantially reduce the

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amount of electrical energy required to sustain the non-thermal plasma. According to a particular embodiment, the reducing agent is  $H_2$  when the halogen-containing gas is  $F_2$ .

The relative amount of reducing agent mixed with the halogen-containing gas may vary considerably. According to a particular embodiment, the relative amount may vary from about 0.5:1 to about 4:1  $H_2$ :halogen atom molar ratio. In the case of  $H_2$  as the reducing agent and  $F_2$  as the halogen-containing gas, the molar ratio may be about 1:1 (which equates to 1:1 by volume concentration ratio). In particular, the volume concentration of  $H_2$  introduced into the  $F_2$ -containing treatment gas may be at least equal to the volume concentration of  $F_2$ . Avoiding possible explosive conditions is also a consideration in the  $F_2/H_2$  mix ratio. Options for eliminating explosive conditions may include diluting the  $H_2$  with an inert gas, adding  $H_2$  gradually to the  $F_2$ -containing stream, and adding excess  $H_2$  above the amount that could be consumed in the reduction reaction.

The reducing agent may be mixed with the halogen-containing gas in any suitable manner. Complete mixing may be achieved prior to generating the plasma. Alternatively, the reducing agent may be gradually mixed with the halogen-containing gas during plasma generation. Such gradual mixing may reduce exothermic heat generation and assist in avoiding explosive conditions. The mixing may be accomplished with any known mixing procedures or devices such as, for example, static mixing, nozzles, baffles or a packed bed.

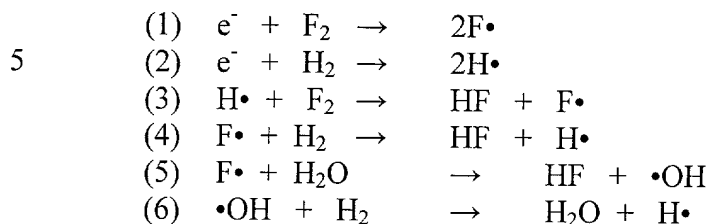
The temperature and pressure of the treatment gas and the reducing agent at the point of mixing are not critical. The treatment gas, for example, can be at the temperature and pressure that exist in the effluent stream from any processing module. Typically, the treatment gas and the reducing agent are at ambient temperature and pressure.

Although not bound by any theory, it is believed that the reducing agent reduces the halogen-containing gas via a reaction involving generating a hydrogen radical ( $H\bullet$ ) in the presence of the plasma. The hydrogen radicals dissociate a free halide gas (e.g.,  $F_2$ ) or react with a halogen atom in a halogenated hydrocarbon. By way of example, a



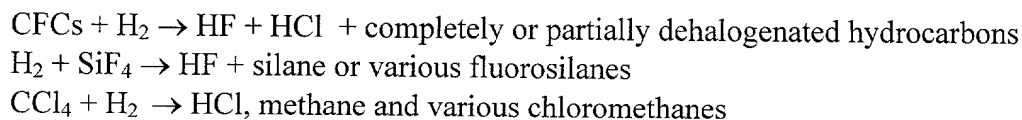
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disassociative reduction pathway is illustrated below with reference to F<sub>2</sub> reduction by H<sub>2</sub> in a non-thermal reactor in the presence of water.

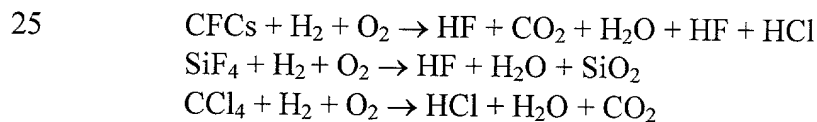


The chain propagation depicted above, in essence, provides a continuous source of hydrogen radicals that requires less energy to generate than in the case of employing water alone as the reducing agent. It should be noted that reactions (5) and (6) are optional since the presence of water is not required in all of the disclosed embodiments.

15 Other possible specific reductions and reduction products include:



It is also possible to add O<sub>2</sub> to the feed gas mixture in the plasma in these reductions to oxidize the hydrocarbons. The complete reactions then would be:



Reduction of other halogen-containing feed gas can result in a variety of  
30 additional gaseous reduction products.

According to certain embodiments of the processes, at least one of the reduction products for each particular halogen-containing treatment gas is substantially water-soluble or at least more water-soluble than the halogen-containing treatment gas. Such

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water-soluble gaseous reduction products can be dissolved in water for further treatment. For example, HF gas can be scrubbed and the resulting HF-containing water can be neutralized with a base. One particular neutralization method for HF acid involves treating the HF acid in a calcium or sodium alkaline scrubber to produce calcium or sodium fluoride. The calcium or sodium fluoride may be subsequently processed and sent to a landfill or used as an additive for dental treatments. Other separation techniques such as a water bubbler or water spray contactor may also be used for removing gaseous reduction products that are not intended for emission into the atmosphere. As described in more detail below, the scrubbing of the gaseous reduction product may occur at least partially within the plasma reactor. Alternatively, the scrubbing may be performed downstream from the plasma reactor in a separate unit. Such scrubbing is well-known and any suitable devices or processes may be used.

The liquid present during the plasma generation and reduction reaction may be any liquid that has heat absorbing and gas-solvating characteristics. Illustrative heat-absorbing liquids include those that have a low boiling point such as, for example, less than about 150°C and a high heat of vaporization such as, for example, at least about 35 kJ/mole. Water is the typical liquid, but other liquids such as alcohols, light oils, waxes or other hydrocarbons may be used. When F<sub>2</sub> is the treatment gas the water may include particles of calcium hydroxide in the form of a slurry or may be a solution of sodium hydroxide. Calcium hydroxide and sodium hydroxide react with HF and, thus, would promote additional scrubbing of the HF from the product gas stream in the plasma reactor. The heat absorbed by the liquid water causes at least a portion of the liquid water to evaporate into the gas phase (i.e., steam). This heat absorption/evaporation mechanism prevents significant increases in the temperature of the bulk gas mixture undergoing treatment. For example, in certain embodiments the temperature of the bulk gas mixture does not exceed about 100°C. Since no heat is externally applied or generated by the plasma itself, the overall operating conditions of these embodiments does not exceed about 100°C.

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The plasma may be generated by any energy supply source known in the art. For example, the plasma could be energized by radio frequency (RF), microwave, laser, electrical discharge, or a combination thereof. Myriad reactor configurations are known for each type of plasma and any such geometry may be suitable for effecting the disclosed processes. According to particular embodiments of the disclosed processes, the plasma is a non-thermal plasma.

A basic distinction between non-thermal plasmas and thermal plasmas is described above. Other possible characteristics of non-thermal plasmas are that some non-thermal reactors have a relatively small footprint since they operate at atmospheric pressure. In addition, the power sources are relatively simple AC or DC sources.

The plasma operating conditions may vary depending upon the type of plasma employed. Non-thermal plasmas typically operate from sub-ambient temperature up to at least about 600°C, but the temperature of the bulk gas in the plasma may vary depending on the temperature of the incoming feed gas or as the result of any enthalpy released from the chemical reactions occurring in the plasma. For example, the disclosed reduction of F<sub>2</sub> is an exothermic reaction and, thus, the temperature of the bulk gas in the plasma may rise to about 500 or 600°C. However, this temperature can be reduced to less than or equal to about 100°C by generating the plasma in the presence of a liquid that can absorb the heat as described below in more detail.

The operating pressure for non-thermal plasmas may vary. For example, glow discharge non-thermal pressures typically operate at subatmospheric pressures such as, for example, about 1 mTorr to about 50 Torr. Silent discharge reactors and pulsed-DC reactors (described below in more detail) typically operate at slightly sub-ambient to slightly above-ambient pressure such as, for example, about 0.5 atmospheres to about 10 atmospheres. The power required to generate the non-thermal plasma may vary depending upon the feed gas flow rate and the type of halogen-containing gas undergoing treatment. It is known that, in general, the specific power may be calculated by the equation: (volume flow rate x energy/volume = power). For example, in the embodiment of about 1:1 H<sub>2</sub>:F<sub>2</sub> volume % in the feed gas stream, substantially complete

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reduction of  $F_2$  occurs at about 80 to about 150 J/L feed gas. This equates to approximately 1 kW of power required per 400 L/minute of feed gas.

Although any type of non-thermal plasma-generating system may be utilized for the disclosed processes, there are two types that may be especially suitable since they are capable of generating non-thermal plasmas at ambient pressure. These two non-thermal plasma-generation systems are referred to herein as a silent discharge reactor (also known in the art as "dielectric barrier discharge reactor") and a pulsed-DC reactor, respectively. The general geometry and operation of such reactors is described below. An additional, particularly useful, plasma reactor embodiment is referred to herein as a "film discharge reactor". It should be recognized that film discharge reactors may be useful regardless of the type of plasma-generation system employed. In other words, a silent discharge system may be combined with film discharge reactor geometry resulting in a silent-discharge, film reactor. The general geometry and operation of a film discharge reactor is also described below.

In a silent discharge reactor, at least one high voltage electrode is located a distance from at least one opposing ground electrode. The gaps between the high voltage electrodes and the opposing ground electrodes define a passage through which a gas flows. A dielectric material is disposed on the surface of the high voltage and/or ground electrodes. A voltage is applied to the high voltage electrode to generate a non-thermal plasma discharge in the gap between the high voltage electrode and the ground electrode. The non-thermal plasma is maintained by applying an AC voltage to the high voltage electrode.

In a pulsed-DC reactor, a high voltage electrode is located a distance from an opposing ground electrode. The gap between the high voltage electrode and the opposing ground electrode defines a passage through which a gas flows. There is no dielectric material disposed on any surface. A voltage is applied to the high voltage electrode to generate a non-thermal plasma discharge in at least a portion of the gap between the high voltage electrode and the ground electrode. The non-thermal plasma is maintained by applying a pulsed DC voltage to the high voltage electrode. The

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pulsed DC voltage ramps up and down very quickly (e.g., a nanosecond). In general, pulsed-DC reactor systems tend to be more expensive than silent discharge reactors due to the relatively elaborate power supply configuration required for pulsed-DC reactors.

In both the silent discharge reactor and the pulsed-DC reactor, when the electric field reaches a sufficient level, electrons are accelerated to the point that they will collide with, and ionize, gas molecules. Each such collision produces a charged molecule (i.e., ion) and one additional electron. This continuing process multiplies the number of electrons in the gap (referred to in the art as "avalanches"). In the case of a silent discharge reactor the avalanches (also known as "micro-streamers") continues until it impacts a dielectric material barrier. The charge accumulation at the dielectric material barrier effectively terminates the avalanche in order to avoid formation of an arc that would lead to generation of a thermal plasma. When the AC polarity at the high voltage electrode reverse, the process repeats itself. In the case of a pulsed-DC reactor, the end of the DC pulse extinguishes each avalanche. The electrons generated in such plasmas react with the gases in the gap as described above.

In a film discharge reactor, a first electrode is located a distance from a film or body of liquid that contacts or immerses an opposing second electrode or a dielectric barrier disposed on the second electrode (referred to herein as the "wetted electrode"). The liquid film may be flowing over at least a portion of the boundary of the second electrode. Alternatively, the second electrode may be disposed in a liquid bath or reservoir that may or may not be flowing. The space between the first electrode and the opposing second electrode defines a passage through which a treatment gas flows. According to the disclosed processes, the treatment gas flows over the surface of the liquid and a plasma is generated in the gas region between the first electrode and the liquid surface, particularly at or near the surface of the liquid. The plasma radicals and the reduction products may contact the surface of the liquid. The liquid in a film discharge reactor can absorb the heat generated by the exothermic reduction reaction and can at least initially dissolve the water-soluble reaction products as mentioned above.

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The plasma can be generated in a device containing any type of geometrical-shaped electrodes. General classes of potential devices include parallel plate (horizontal or vertical) reactors, cylindrical plasma reactors, and reactors containing arrays of tubular electrodes. One example of a possible non-thermal, film discharge reactor configuration is shown in U.S. Patent No. 5,980,701. A few particular embodiments of possible non-thermal, film discharge reactors are described below.

One embodiment of a non-thermal, film discharge reactor is shown in FIG. 1. A chamber 10 defines an upper portion 11, a lower portion 12, side wall 15, top wall 22, bottom wall 23, and an interior void 18. The chamber 10 depicted in FIG. 1 is cylindrical but it could be another shape such as conical or rectangular. At least one first electrode 13 is received within the upper portion 11 of the chamber 10. A dielectric barrier coating or sheath 14 is disposed on the surface of the first electrode 13. The dielectric barrier coating 14 may encapsulate all or a substantial portion of the first electrode 13. The first electrode 13 may be made from any type of conductive material known in the art such as, for example, graphite, vitreous carbon, stainless steel, or other metals, or a conductive salt solution. The dielectric barrier coating 14 may be made from any type of known dielectric material such as alumina, perfluorinated polyethylene, quartz, glass, or other metal oxides. The dielectric barrier coating 14 should be sufficiently thick to prevent dielectric breakdown of the dielectric material at the operating fields of the device. The first electrode 13 coated with the dielectric barrier 14 may have any shape such as an elongated rod, a wire or an elongated plate.

At least one second electrode 16 is located at the side-walls 15 of the chamber 10. The second electrode 16 is disposed within the chamber 10 in the sense that it may define the side-walls 15 or it could be disposed on an inside surface 17 of the side-walls 15. The second electrode 16 may have any shape such as a tubular plate extending around the circumference of the cylindrical chamber 10, circular rods extending around the circumference of the cylindrical chamber 10, an elongated, substantially planar plate, or a porous material such as a fabric or foam-like material. Although not shown, the second electrode 16 may include a dielectric barrier coating or sheath.

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According to the embodiment of FIG. 1 an AC voltage source (not shown) is operatively coupled to first electrode **13** and the second electrode **16** is grounded (or connected to a low voltage source (not shown)). Thus, first electrode **13** is the high voltage or "hot" electrode and the second electrode **16** is the ground electrode.

5 Alternatively, the AC voltage source could be coupled to the second electrode **16** and the first electrode **13** could serve as the ground electrode. The first electrode **13** and the second electrode **16** are positioned in an opposing relationship so that an electric field can be generated in the void or gap between the first electrode **13** and the second electrode **16**.

10 In general, the plasma reactor chamber defines at least one inlet for introducing a feed gas into the interior void of the chamber. According to one variant (not shown), there are only inlets for receiving a feed gas that is a mixture of the treatment gas and the reducing agent gas. In other words, the treatment gas and the reducing agent gas are pre-mixed prior to entering the plasma reactor chamber. According to another variant  
15 (depicted in FIG. 1), the treatment gas and the reducing agent are mixed in the plasma reaction chamber. Of course, pre-mixing and in-chamber mixing could both be used in a system.

In particular, there is at least one inlet **19** for introducing the treatment gas into the interior void **18** of the chamber **10**. Inlet **19** may be located at any position in the  
20 chamber such as the top wall **22** of the chamber **10** as illustrated in FIG. 1 or in the bottom wall **23** of the chamber **10**. Another option is to provide a first electrode **13** that defines pinholes for introducing the treatment gas. Inlet **19** is in fluid communication with a source of treatment gas.

There is also at least one inlet **20** for introducing the reducing agent into the  
25 interior void **18** of the chamber **10**. Inlet **20** also may be located at any position in the chamber **10**. In the FIG. 1 embodiment, the side-walls **15** and second electrode **16** define inlets **20**. For example, the side-walls **15** and/or second electrode **16** can be made of a porous or foam-like material or they can define pinholes through which the reducing agent gas can flow. In the case of the side-walls **15**, the porous material can

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be made of alumina, perfluorinated polyethylene (e.g., Teflon®), glass or other metal oxides. The inlets **20** may be arranged along the axial length of the cylindrical chamber **10** so that the reducing agent can be gradually introduced into the treatment gas stream as it flows through the chamber **10**. Inlet **20** is in fluid communication with a reducing agent source.

The interior void **18** of the chamber **10** includes a liquid region **21** that is contiguous with the inside surface **17** of the side-walls **15** and partially fills the interior void **18**. The liquid region includes a liquid surface **30** facing the interior void **18** of the chamber **10**. A heat-absorbing liquid such as described above occupies liquid region **21** during operation of the plasma reactor. The liquid region **21** depicted in FIG. 1 is in the form of a liquid film that gravity flows along the inside surface **17** of the side-walls **15**. The liquid film is maintained within liquid region **21** via surface tension. The inside surface **17** of the side-walls **15** may be provided with grooves or other types of texturing for promoting the uniformity of the liquid film.

Two examples of side-wall **15**/liquid region **21** configurations are shown in FIGS. 2 and 3, respectively. Both FIGS. 2 and 3 illustrate horizontal electrode embodiments as opposed to the cylindrical vertical embodiment of FIG. 1. But the ground electrode, liquid region and reducing agent introduction arrangements depicted in FIGS. 2 and 3 may also be utilized for the side-wall **15**/liquid region **21** of FIG. 1. In particular, the design in FIG. 2 is provided with a first section **50** that includes first electrodes **51**, a diffuser **52** through which the reducing agent can flow, and a liquid region **53**. The first section **50** is an example of a possible arrangement for the side-wall **15**/liquid region **21** of FIG. 1. Similarly, the design in FIG. 3 is provided with a first section **70** that includes first electrodes **71**, a liquid region **72**, and an electrochemical cell **73** for producing a reducing agent gas. The embodiments shown in FIGS. 2 and 3 are described below in more detail.

Referring back to FIG. 1, the top wall **22** of the chamber **10** defines an inlet port **24** for introducing the liquid into the liquid region **21**. The bottom wall **23** of the



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chamber **10** defines an outlet port **26** through which the liquid exits from the chamber **10**.

The interior void **18** of the chamber **10** also includes a gas-scrubbing region **27** that is populated with gas-scrubbing packing material **28**. The gas-scrubbing packing material **28** may be any type of material that is known to provide increased surface area for gas/liquid exchange. Illustrative gas-scrubbing packing material particularly suitable for HF include perfluorinated polymeric materials such as perfluorinated polyethylenes or polyvinylidene fluoride. Liquid may be provided to the gas-scrubbing packing material **28** by draining the liquid from the liquid region **21** through the gas-scrubbing packing material **28**. Optional liquid sprayers **25** may also be provided at the side- walls **15** of the chamber **10**.

The chamber **10** also includes at least one outlet **29** for exhausting the product gas mixture from the chamber **10**. The outlet **29** may be located at any position in the chamber **10** such as, for example, in the lower portion **12** of the chamber **10** as shown in FIG. 1. In a variant that has the treatment gas inlet **19** located in the lower portion **13** of the chamber **10**, the exhaust or product gas outlet **29** typically is located in the upper portion **11** of the chamber **10**.

During operation of the plasma reactor of FIG. 1 a treatment gas will flow through inlets **19** and then vertically down along the length of void **18** in the chamber **10**. The treatment gas includes a halogen-containing gas such as  $F_2$  and may include other gases such as  $N_2$ . A reducing agent gas such as  $H_2$  will flow through inlets **20** and into void **18** of the chamber **10**. The reducing agent gas flowing through inlets **20** bubbles through the liquid in the liquid region **21** and mixes into the treatment gas stream forming a feed gas stream. A liquid such as water may also be flowing through the liquid region **21**. Thus, the liquid and the gas may be flowing in the same direction through the chamber **10** (i.e., co-current flow). The flow rate of the treatment gas, reducing agent gas, resulting feed gas mixture, and liquid may vary widely depending upon the desired amount of treatment gas for abatement. For example, the flow rate of

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the feed gas mixture through the chamber **10** may be from about 100 standard cubic centimeters per minute (sccm) to about 1500 standard liters per minute.

Electric power will be supplied from the AC voltage source to the first electrode **13** to generate a non-thermal plasma in the feed gas mixture present in the gap between the first electrode **13** and the second electrode **16**. The frequency applied to the first electrode **13** may vary depending upon the feed gas flow rate and halogen concentration. The applied frequency, for example, may range from about 50 Hz to about 2000 Hz, particularly about 100 Hz to about 1000 Hz. The voltage applied to the first electrode **13** may vary depending on the gap distance between the first electrode **13** and the second electrode **16**, the types of gas in the feed gas, and the temperature and pressure of the system. The applied voltage should be sufficient to at least reach onset voltage as is understood in the art. As an example, a voltage of about 10 to about 30 kV may be applied to the first electrode **13** when the feed gas is a mixture of F<sub>2</sub>, N<sub>2</sub> and H<sub>2</sub> and the electrode gap is about 0.1 to about 3 cm.

The reduction reaction in the plasma-excited feed gas mixture will occur at or near the interior surface **30** of the liquid region **21**. Consequently, the exothermic heat from the reduction reaction will be absorbed by the liquid in the liquid region **21**. The heat absorption may be sufficient to vaporize a portion of the liquid, but the continuous feed of flowing liquid will replace any vaporized portion. The vaporized liquid (e.g., steam) enters the void **18** of the chamber **10** and is exhausted with the product gas stream via exhaust gas outlets **29**.

At least a portion of the water-soluble gaseous reduction product (such as HF) formed in the void **18** of the chamber **10** will be scrubbed from the gas stream as it progresses down the vertical axial length of chamber **10**. In particular, a portion of the gaseous reduction product may dissolve in the liquid of the liquid region **21** as it flows down the inside surface **17** of the side wall **15**. A portion of the gaseous reduction product also dissolves in the liquid provided in the gas-scrubbing region **27**.

The exhaust gas exiting through outlet **29** may include any reduction reaction product that was not removed from the scrubbing action in the chamber **10** (such as

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HF), non-reducible gases that were present in the treatment gas (such as N<sub>2</sub>), and excess reducing agent (such as H<sub>2</sub>). The liquid exiting through outlet port **26** may include dissolved reduction products (such as HF).

It will be appreciated that there could be variations of a cylindrical, non-thermal, film discharge reactor similar to that depicted in FIG. 1. For example, the treatment gas could flow into the chamber at the bottom of the chamber and the product gas exit at the top of the chamber. In such a variant, the liquid flowing down the inside surface **17** of the side wall **15** will be moving countercurrent to the flow of the gas. This may provide improved absorption of the reduction product into the liquid.

Another option is to not provide the scrubbing packing material **28** in the interior void **18** of the chamber. In this case, partial scrubbing of the reduction product in the liquid of the liquid region **21** likely will occur, but the product gas exhausting from the chamber will include a greater concentration of reduction product gas. Such remaining reaction product gas could simply be scrubbed in a downstream module.

As mentioned above, both FIGS. 2 and 3 illustrate examples of the electrode arrangement in horizontal, silent-discharge, film reactors. FIG. 2 depicts an embodiment wherein the reducing agent gas is supplied from a source (not shown) external to the reactor. FIG. 3 shows an alternative approach for supplying the reducing agent that involves integrating an electrochemical cell into the plasma reactor structure. Another possibility is to provide the plasma reactor with a H<sub>2</sub> reformer.

In particular, FIG. 2 depicts first electrodes **51** that are surrounded by a liquid region **53**. The liquid region **53** is bounded or supported on a lower side **54** by a diffuser **52**. The liquid region **53** has an upper surface **55**. Second electrodes **56** are located a distance above the upper surface **55** of the liquid region **53** in an opposing relationship relative to the first electrodes **51**. A dielectric barrier coating or sheath **57** is disposed on the surface of second electrodes **56**. The first and second electrodes **51** and **56**, dielectric barrier **57**, and liquid in the liquid region **53** may be comprised of the same materials as described above in connection with FIG. 1. The diffuser **52** may be made of any porous or foam-like material that includes microvoids for allowing passage

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of reducing agent gas molecules **58** to bubble into the liquid. In FIG. 2, first and second electrodes **51** and **56** are in the shape of cylindrical rods, but both or either electrodes **51** and **56** could have other shapes such as, for example, planar plates. If first electrode **51** is planar in shape it can be provided with pinholes or microvoids (such as in a porous material or mesh) for allowing passage of the reducing agent gas. It will be understood that the rod-shaped electrodes **51** and **56** have an axial length extending out from, and into, the plane of the drawing surface of FIG. 2.

It will be appreciated that the representation in FIGS. 2 shows only a portion of a horizontal plasma reactor. First region **50** and second electrodes **56** may be housed inside a chamber. The rod-shaped electrodes **51** and **56**, and the diffuser **52** may be connected to a wall of such chamber for support. The chamber, of course, would include inlets and outlets for the treatment gas, reducing agent gas, product or exhaust gas and the liquid. An AC voltage source (not shown) is operatively coupled to second electrodes **56** and the first electrodes **51** are grounded (or connected to a low voltage source (not shown)). Thus, second electrodes **56** are the high voltage or "hot" electrode and the first electrodes **51** are the ground electrodes. Alternatively, the AC voltage source could be coupled to the first electrodes **51** and the second electrodes **56** could serve as the ground electrodes. The first electrodes **51** and the second electrode **56** are positioned in an opposing relationship so that an electromagnetic field can be generated in the void or gap **59** between the first electrodes **51** and the upper surface **55** of the liquid region **53**.

During operation a treatment gas will flow in the gap **59** and mix with reducing agent gas bubbling out of the upper surface **55** of the liquid flowing through the liquid region **53** to form a feed gas mixture. A silent discharge plasma will be generated in the feed gas mixture in the gap **59** to initiate and sustain the reduction of the halogen gas in the treatment gas. The resulting product gas then will exit the chamber via an exhaust gas outlet. The feed gas flow direction and liquid flow direction may both be parallel along the axial length of the electrodes **51** and **56** (i.e., co-current flow) or there may be countercurrent flow. Alternatively, the feed gas flow direction and the liquid flow

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direction may be perpendicular (or at some other angle) relative to the each other. In this case, either the feed gas flow direction or the liquid flow direction would be perpendicular or angled relative to the axial length of the electrodes **51** and **56**.

FIG. 3 depicts first electrodes **71** that are surrounded by a first liquid region **72**.

5 An electrochemical cell **73** for generating a reducing agent such as  $H_2$  is located adjacent to the first liquid region **72**. The electrochemical cell **73** includes an electrochemical ground electrode **74**, a membrane **75**, and a cathode **76** and is immersed in a second liquid region **77** (e.g., water). The electrochemical cell **73** generates  $H_2$  molecules **78** and  $O_2$  molecules **79** based on well known principles. The membrane **75**  
10 may be angled relative to the plane of the cathode **76** to flow the  $O_2$  molecules **79** in the direction indicated in FIG. 3. The electrochemical ground electrode **74** and cathode **76** may be made from any type of conductive material known in the art such as, for example, graphite, vitreous carbon, stainless steel, other metals, or a conductive salt solution. The membrane **75** may be made from any ion exchange material known in the  
15 art such as, for example, perfluorinated polymers (e.g., Nafion® available from E.I. du Pont).

Electrochemical ground electrode **74** partitions first liquid region **72** and second liquid region **77**. The respective liquids in first liquid region **72** and second liquid region **77** may be the same or different. According to a particular embodiment, the  
20 liquid is water in both first liquid region **72** and second liquid region **77**.

The first liquid region **72** may be bounded or supported on a lower side **80** by the electrochemical ground electrode **74**. The first liquid region **72** has an upper surface. Second electrodes **82** are located a distance above the upper surface **81** of the first liquid region **72** in an opposing relationship relative to the first electrodes **71**. A  
25 dielectric barrier coating or sheath **83** is disposed on the surface of second electrodes **82**. The first and second electrodes **71** and **82**, dielectric barrier **83**, and liquid in the first liquid region **72** may be comprised of the same materials as described above in connection with FIG. 1. In FIG. 3, first and second electrodes **71** and **82** are in the shape of cylindrical rods, but both or either electrodes **71** and **82** could have other

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shapes such as, for example, planar plates. If first electrode 71 is planar in shape it can be provided with pinholes or microvoids (such as in a porous material or mesh) for allowing passage of the reducing agent gas. It will be understood that the rod-shaped electrodes 71 and 82 have an axial length extending out from, and into, the plane of the drawing surface of FIG. 3.

It will be appreciated that the representation in FIGS. 3 shows only a portion of a horizontal plasma reactor. First region 70, second electrodes 82 and electrochemical cell 73 may be housed inside a chamber. The rod-shaped electrodes 71 and 82, and the electrochemical cell 73 parts may be connected to a wall of such chamber for support.

The chamber, of course, would include inlets and outlets for the treatment gas, reducing agent gas, product or exhaust gas and the liquids. An AC voltage source (not shown) is operatively coupled to second electrodes 82 and the first electrodes 71 are grounded (or connected to a low voltage source (not shown)). Thus, second electrodes 82 are the high voltage or "hot" electrode and the first electrodes 71 are the ground electrodes.

Alternatively, the AC voltage source could be coupled to the first electrodes 71 and the second electrodes 82 could serve as the ground electrodes. The first electrodes 71 and the second electrode 82 are positioned in an opposing relationship so that an electromagnetic field can be generated in the void or gap 84 between the first electrodes 71 and the upper surface 81 of the first liquid region 72. A DC power supply that operates at low voltage and moderate current may be coupled to the electrochemical cathode 76.

During operation a treatment gas will flow in the gap 84 and mix with reducing agent gas bubbling out of the upper surface 81 of the liquid flowing through the liquid region 72 to form a feed gas mixture. A silent discharge plasma will be generated in the feed gas mixture in the gap 84 to initiate and sustain the reduction of the halogen gas in the treatment gas. The resulting product gas then will exit the chamber via an exhaust gas outlet. The feed gas flow direction and liquid flow direction may both be parallel along the axial length of the electrodes 71 and 82 (i.e., co-current flow) or there may be countercurrent flow. Alternatively, the feed gas flow direction and the liquid flow

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direction may be perpendicular (or at some other angle) relative to the each other. In this case, either the feed gas flow direction or the liquid flow direction would be perpendicular or angled relative to the axial length of the electrodes **71** and **82**.

Another silent discharge plasma reactor that can be used to perform the disclosed processes is represented in FIG. 4. An inner cylindrical electrode **100** is received within an outer tubular electrode **101**. The outer cylindrical electrode **101** defines an inner surface **102** that supports a first dielectric barrier **103**. The inner cylindrical electrode **100** defines an outer peripheral surface **104** that supports a second dielectric barrier **105**. The inner surface **102** of the outer electrode **101** and the outer surface of **104** of the inner cylindrical electrode **100** define an annular gap **106**. According to another embodiment, only one of the first or second dielectric barriers **103**, **105** is present. A dielectric packing material may be received within at least a portion of the annular gap **106**. Illustrative dielectric packing materials include quartz, alumina, titania, other non-conductive ceramics, and fluorinated polymers. The electrodes **100** and **101** and the dielectric barriers **103** and **105** may be made with any of the materials described above in connection with the embodiments shown in FIGS 1-3.

An AC voltage source (not shown) is operatively coupled to inner cylindrical electrode **100** and the outer tubular electrode **101** is grounded (or connected to a low voltage source (not shown)). Thus, inner cylindrical electrode **100** is the high voltage or “hot” electrode and the outer tubular electrode **101** is the ground electrode. Alternatively, the AC voltage source could be coupled to the outer tubular electrode **101** and the inner cylindrical electrode **100** could serve as the ground electrode. An electromagnetic field can be generated in the annular gap **106**.

During operation a feed gas mixture that includes the treatment gas and the reducing agent gas enters the reactor through an inlet (not shown) and flows through the annular gap **106**. A silent discharge plasma is generated in the feed gas mixture in the annular gap **106** to initiate and sustain the reduction of the halogen gas in the treatment gas. The resulting product gas then will exit the reactor via an exhaust gas outlet (not shown).

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As described above, the corrosive effect of the reduction products such as HF is substantially diminished at the lower operating temperatures of the disclosed processes. One consequence is that HF-resistant materials such as fluorinated polymers (e.g., Teflon® perfluorinated polyethylenes or polyvinylidene fluoride) can be used for parts of the plasma reactor or to coat exposed surfaces of the plasma reactor. Such materials tend to be less expensive than the specialized corrosion-resistant metal alloys required in harsher environments resulting from higher temperatures.

The plasma reactor may be connected to the various gas and liquid sources and exhaust gas treatment modules by any known means. FIG. 5 depicts one example of a system that includes a silent-discharge, film reactor. It will be appreciated that there may be alternative arrangements of the various components of the system shown in FIG. 5. The system may also include further components such as additional gas sources or control devices such as pumps and valves.

With specific reference to FIG. 5, there is provided a treatment gas source **120** and a reducing agent source **121**. The treatment gas source **120** and the reducing agent source **121** are connected to conduits **122** and **123**, respectively. Conduits **122** and **123** converge in a gas-mixing zone **124**. The gas-mixing zone **124** is connected to a silent-discharge, film-discharge reactor **126** via gas conduit **125**.

The reactor **126** includes at least one feed gas inlet **127** and at least one exhaust or product gas outlet **128**. The exhaust gas outlet **128** is connected to a water-scrubbing unit **144** via gas conduit **145**. The reactor **126** also includes a first plate electrode **129** and a second plate electrode **130** that are positioned in an opposing relationship. The first electrode **129** is operatively coupled to an AC voltage source **131** and the second electrode **130** is grounded (or connected to a low voltage source (not shown)). The first electrode **129** has an inner surface **132** upon which is disposed a first dielectric barrier **133**. The second electrode **130** has an inner surface **134** upon which is disposed a second dielectric barrier **135**. A liquid film **136** flows along the length of an inner surface **137** of the first dielectric barrier **133**. A gap **146** is defined between an inner surface **147** of the liquid film **136** and an inner surface **148** of the second dielectric



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barrier **135**. The electrodes **129**, **130**, dielectric barriers **133**, **135**, and liquid film **136** may be made from the materials described above.

The reactor **126** includes an inlet port **138** and an outlet port **139** for the liquid. The outlet port **139** may be fluidly connected to a liquid reservoir **140**. The liquid  
5 reservoir **140** is fluidly connected to the inlet port **138** via a liquid recycling loop **141**. A fresh liquid source **142** and a liquid purge conduit **143** are fluidly connected to the liquid recycling loop **141**.

During operation the treatment gas (e.g.  $F_2/N_2$ ) flowing through gas conduit **122** will mix in the gas-mixing zone **124** with the reducing agent gas (e.g.,  $H_2$ ) flowing  
10 through conduit **123**. The resulting feed gas mixture from the gas-mixing zone **124** will flow through conduit **125** and gas inlet **127** into gap **146** of the reactor **126**. An AC voltage will be applied to the first electrode **129** to generate a non-thermal plasma in the feed gas mixture flowing through the gap **146**. The liquid film **136** (e.g., water) will flow down along the length of the inner surface **137** of the first dielectric barrier **133**.  
15 The reduction reaction in the non-thermal plasma will occur at or near the inner surface **147** of the liquid film **136**. The heat produced by the reduction reaction may be absorbed by the liquid film **136**. In addition, water-soluble reaction products (e.g., HF) may dissolve into the liquid film **136**. Liquid that includes a sufficient concentration of dissolved reaction products may be removed from the system via the liquid purge  
20 conduit **143**. The gas exiting the reactor **126** through the exhaust gas outlet **128** may include reaction products (e.g., HF) and any non-reacted inert gases (e.g.,  $N_2$ ). The water-soluble reaction product(s) are then treated in the water-scrubbing unit **144**.

Control of such a system exemplified by FIG. 5 may be implemented by any of the techniques well known in process control. For example, a sensor may be placed in  
25 an appropriate location in the system to monitor the relevant parameters of the treatment gas, particularly the halogen concentration. Data from this sensor may be inputted into a computer controller that determines the appropriate responsive settings for other operating parameters of the system (e.g., reducing agent concentration, voltage to the

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plasma reactor electrode, water flow rate, etc.). The controller then generates instruction signals to the control devices for each such operating parameter.

One such sensor could be placed at the treatment gas inlet into the chamber for measuring the halogen concentration and adjusting the amount of reducing agent and liquid flow rate accordingly. For example, in the system of FIG. 5 a sensor for detecting halogen concentration may be operatively coupled to gas conduits **122**, **123** and/or **125** and to liquid recycling loop **141**. Another useful parameter for monitoring may be the voltage and current measured from the high voltage electrode to the ground electrode. For example, in the system of FIG. 5 a voltage probe may be operatively coupled to the first electrode **129** and a sensing capacitor may be operatively coupled to the second electrode **130**. A method for obtaining the plasma power input with such a probe-and-capacitor arrangement is described in Rosenthal, L. and Davis, D., "Corona Discharge for Surface Treatment", IEEE Transactions of Industry Applications, I-5, 328 (May/June 1975).

As mentioned above, the disclosed process is especially suitable for treatment of effluent streams from semiconductor manufacturing processes such as plasma etch, plasma-enhanced chemical vapor deposition and plasma-assisted chamber cleaning processes. In such manufacturing processes there is often a dry or roughing pump or similar device located downstream of the etch or deposition process tool that dilutes the effluent with an inert gas such as nitrogen. According to one embodiment of the disclosed process, the plasma reactor for carrying out the process is located downstream from such an inert gas source and, thus, N<sub>2</sub> (or other inert gas) constitutes a substantial portion of the treatment feed gas mixture. In other words, this specific embodiment is not a so-called "point-of use" abatement system since it is not treating the effluent stream immediately after it exists the etch or deposition chamber.

The specific examples described below are for illustrative purposes and should not be considered as limiting the scope of this disclosure.

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### Example 1

A treatment gas containing 1000 ppm F<sub>2</sub> in N<sub>2</sub> background gas was mixed with various H<sub>2</sub> streams (at a 1:1 H<sub>2</sub>:F<sub>2</sub> molar ratio and a 2:1 H<sub>2</sub>:F<sub>2</sub> molar ratio). The treatment gas and H<sub>2</sub> were supplied at ambient temperature and pressure. The resulting feed gas mixtures were introduced into the annular gap of a silent discharge plasma reactor having a configuration as shown in FIG. 4. A non-thermal plasma was generated in the feed gas mixtures with AC voltages having different frequencies applied to the high voltage electrode (400 Hz, 200 Hz and 100 Hz). The reactor temperature ranged from 30-35°C. The resulting amount of F<sub>2</sub> in the exhaust gas stream and energy required is shown in the graph of FIG. 6.

### Example 2

Treatment gases containing 4000, 2000, or 1000 ppm F<sub>2</sub> in N<sub>2</sub> background gas were mixed an H<sub>2</sub> stream at a 2:1 H<sub>2</sub>:F<sub>2</sub> molar ratio. The treatment gas and H<sub>2</sub> were supplied at ambient temperature and pressure. The resulting feed gas mixtures were introduced into the annular gap of a silent discharge plasma reactor having a configuration as shown in FIG. 4. A non-thermal plasma was generated in the feed gas mixtures with a 200 Hz AC voltage applied to the high voltage electrode. The reactor temperature ranged from 30-35°C. The resulting amount of F<sub>2</sub> in the exhaust gas stream and energy required is shown in the graph of FIG. 7.

Having illustrated and described the principles of our disclosure with reference to several embodiments, it should be apparent to those of ordinary skill in the art that the invention may be modified in arrangement and detail without departing from such principles.